

HUNGARY

MATE, Janos, Dr, physician-lieutenant colonel, candidate of medical sciences; [affiliation not given].

"The Importance of the Use of Vaccinations in the Current Mode of Prevention of Contagious Diseases in the Armed Forces."

Budapest, Honvedorvos, Vol XV, No 3, July-Sept 1963, pages 204-216.

Abstract: One of the defenses of a possible biological warfare is preventive vaccination. In this connection reference is made to the biological warfare research conducted by the US at Camp Detrick. A peace-time program of preventive vaccination is advocated against the danger of natural infection during wartime as well as against the possible outbreaks which result from biological warfare. The factors which influence the effectiveness of vaccinations are described. Among the techniques, aerogen immunization is considered to be the most suitable for mass treatment. This was developed in Russia but has not become widespread yet. The effect of radiation on immune body production is discussed briefly. Virus immunity and vaccination with viruses is also mentioned. Reports on simultaneous vaccination with various antigens and certain synergistic effects are quoted from the literature. The available vaccination possibilities against most of the diseases which present a danger to adults or may play a role in biological warfare are discussed in detail. The vaccination programs of the French, US, German and Soviet armies are quoted and recommendations made. 24 Eastern European, 19 Western references.

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MATE, Jozsef

The work of the interprofessional committee at Csanadpalota. Munka 11  
no.8:11 Ag '61.

1. Csanadpalotai Szakmakozó Bizottság titkára.

(Hungary—Trade unions)

MATE, K.;PREKOP, D.;ZELLNER, P.

Cortisone treatment of rheumatoid arthritis and a perusal of the present status of the ACTH and cortisone problem. Orv. hetil. 93 no. 11:338-343 16 Mar 1952. (CIML 23:3)

1. Doctors. 2. Department of Internal Medicine (Director -- Head Physician -- Dr. Pal Zellner), Metropolitan Peterffy Sandor-utcai Hospital).

MATE, Karoly, dr.; ZELLNER, Pal, dr.

New facts about the Adams-Stokes syndrome. Orv. hetil. 95 no.28:  
765-766 11 July 54.

1. A Fovarosi Tetenyi-uti Korhaz I. Belosztalyanak (igazgato-  
belgyogyasz foorvos: Zellner Pal, dr.) kozlemenye

(HEART BLOCK

Adams-Stokes synd. with paroxysmal tachycardia, strophanthin-  
diaphyllin-procaine ther.)

(STROPHANTHIN, therapeutic use

Adams-Stokes synd. & ventricular tachycardia, with  
diaphyllin & procaine)

(PROCAINE, therapeutic use

Adams-Stokes synd. & ventricular tachycardia, with  
diaphyllin & strophanthin)

KERTESZ, Tivadarné, dr.,; MATE, Karoly, dr.

Postcholecystography pseudoalbuminuria. Orv. hetil. 96 no.19:  
522 8 May 55

1. A Tetenyi-uti kórház laboratóriumának (először: Paloczky József dr.) és I. belosztályának (először: Zellner Pál dr.) közleménye  
(Elozetes közlemény)

(ALBUMINURIA,

adventitious, postcholecystography)

(CHOLECYSTOGRAPHY, complications,

albuminuria, adventitious)

MATE, Karoly, Dr.; KISKOSZEGI, Andor, Dr.

Clinical data on dermatitides caused by plants and light. Orv. hetil.  
98 no.49:1194-1195 27 Oct 57.

1. A Tetenyi uti Korhaz (igazgato: Zellner Pal dr.) III. sz. Utokeszelo  
Belgyogyaszati Osztalyanak (mb. vezeto: Mate Karoly dr.) es z XIX. ker.  
Bor- es Nemibeteggondozonak (vezeto-foorvos: Temesvary Laszlo dr.)  
kozlemenye.

(DERMATITIS

phytophotodermatitis, clin. data (Hun))

MATE, Károly, Dr.; BATORI, Gabor, Dr.; CSEKE, Janos, Dr.; TRIZNA, Zoltan, Dr.

Use of chlorpromazine in the therapy of emphysema. Orv. hetil. 99 no.24:  
810 15 June 58.

1. A Tetenyi uti Korhaz (igazgato: Zellner Pal dr.) III. sz. Utokezele  
Belosztalyanak kozlemenye.

(EMPHYSEMA, PULMONARY, ther.  
chlorpromazine (Hun))

(CHLORPROMAZINE, ther. use  
emphysema, pulm. (Hun))

MATE, Karoly, dr.

Leprosy. Elovilag 4 no.4:33-38 O-D '59.



MATE, Karoly; SAGI, Bela

Observations on the therapeutic effect of andaxin. Orv. hetil. 100  
no.16:581-582 19 Apr 59.

1. A Tetenyi-uti Korhaz (igazgato: Zellner Pal dr.) III. sz. Belgy-  
ogyaszati Osztalyanak kozlemenye.  
(MEPROBAMATE, ther. use  
clin. evaluation (Run))

KISS, Istvan, dr.; MATE, Karoly, dr.

Simultaneous appearance of thrombocytopenic thrombotic purpura  
and disseminated lupus erythematosus. Orv.hetil. 100 no.43:  
1562-1564 0 '59.

1. A Fov. Tetenyi uti korhaz (ig. foorvos: Zellner Pal dr.)  
III. sz. Belosztelya es Korbonctani osztalyanak (foorvos:  
Kiss Istvan dr.) kozlemenye.

(LUPUS ERYTHEMATOSUS compl.)  
(PURPURA, THROMBOPENIC compl.)



BRANDSTEIN, Laszlo dr.; GREGUSS, Sandor, dr.; LITTMANN, Imre, dr.;  
MATE, Karoly, dr.

Hyperinsulinism diagnosed as epilepsy for several years. (Pancreatic islet cell adenoma). Orv hetil 104 no. 30 28 J1 '63.

1. Fovarosi Tanacs VB. Tetenyi uti Korhaz, I. Sebeszet,  
Idegosztaly es III. Belosztaly.  
(HYPERINSULINISM) (EPILEPSY) (ISLET CELL TUMOR)

MATE, Karoly, dr.; FRIED, Laszlo, dr.

On giant gastric ulcer in old age. Orv. hetil. 105 no.24:  
1114-1118 14 Je'64

1. Fovvrosi Tanacs, Tetenyl uti Korhaz, III. Belosztaly es  
Orvostovabbkepzo Intezet, Rontgenologiai Tansek.

IVANYI, Janos, dr.; FRIED, L.; MATE, K.

Ulcerative diseases in old age. Orv. hetil. 105 no.34:1627  
23 Ag '64.

HANGOS, Gyorgy, dr.; BIRTALAN, Gyozo, dr.; MATE, Karoly, dr.; THURZO, Rezső, dr.

On the treatment of gastroduodenal ulcer in old age. Orv. hetil. 106 no.20:927-928 16 My'65.

1. Orvostovábbképző Intézet, Sebészeti Tanszék, Fővárosi Tünetnyelző Kórház, III. Belosztály és Főv. Csépel Kórház, Sebészeti Osztály.

MATE, L.

From a 2/1 tube radio receiver the "Kanta 573L V" world-wide receiver.

F. 162 (RAD. THE. AREA) In report, Summary Vol. 7, No. 6, Aug. 1951.

SO: Monthly Index of East European Accessions (ab. 1, Vol. 6, No. 11 November 1951)



MATE, L.

On the problem of Mikusinski's logarithm. Mat kut kozl MTA  
7 Ser.A no.1/2:117-124 '62.

MATE, Laszlo

On the expansion of operator semi-groups. Mat kozl MTA 12 no.3:  
217-222 '62.

MATE, Laszlo

The abstract Cauchy problem and operator semigroups. Mat lapok  
13 no.1/2:205-206 '62.

MATE, L.

Semigroup of operators in Frechet space. Dokl. AN SSSR 142  
no.6:1247-1250 F '62. (MIRA 15:2)

1. Politekhnikheskiy institut, Budapesht, Vengerskaya  
Narodnaya Respublika. Predstavleno akademikom V.I.Smirnovym.  
(Spaces, generalized)  
(Operators(Mathematics))

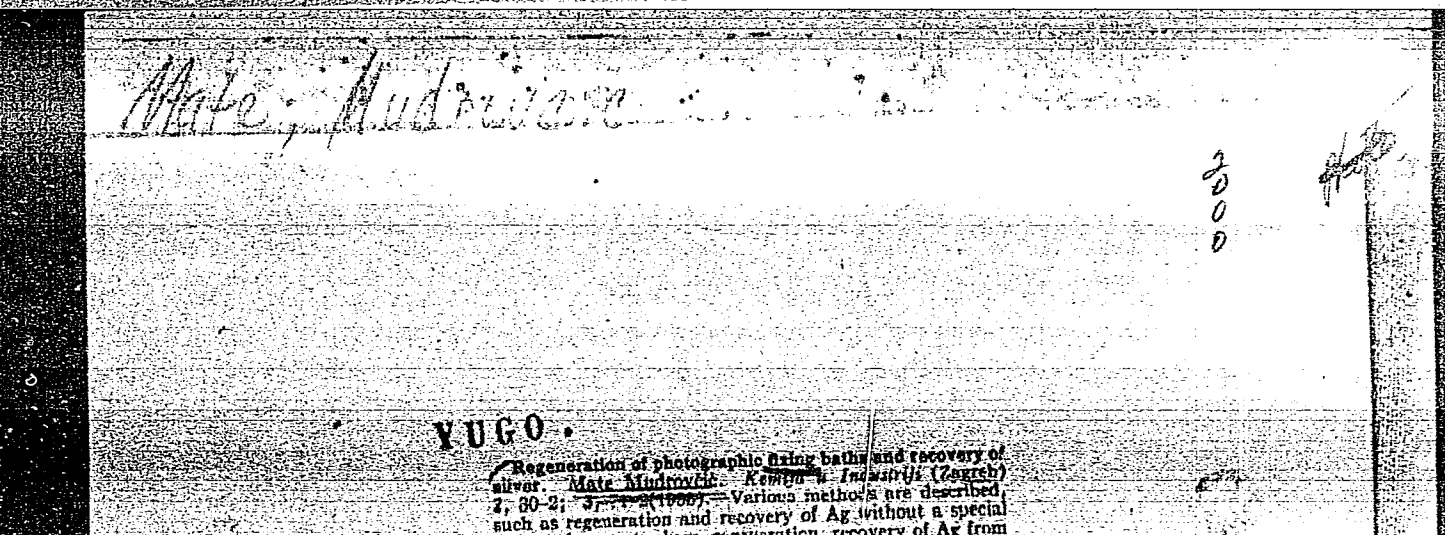
DALLOS, Kalman; MATE, Laszlo

Machine tools with automatic control. Pt.1. Gépgyártastechn  
3 no.5:172-175 My'63.

1. Budapesti Szerszámgépgyár (for Dallos). 2. Finommechanikai Vállalat (for Mate).

SCHMIDT, Egon; STERBETZ, Istvan; GYERESSY, Antal; SCHAFER, Lajos; TERNYAK, Jeno;  
MATE, Laszlo; GEREBY, Gyorgy; BERETZK, Peter, dr.

Data on the avifauna of the region between the Danube and the  
Tisza. Aquila 69/70:258-260 '62-'63 [publ. '64].



"APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R001032820006-9

Ag<sub>2</sub>O ppt., the red coloration of Na<sub>2</sub>SO<sub>4</sub>,  
the recovery of H<sub>2</sub>, and the regeneration of Na<sub>2</sub>SO<sub>4</sub>.

H. A.

was

*[Handwritten signature]*

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APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R001032820006-9"



MATC.M.

1466. Micro-method for detection of mercury  
Kraljic and M. Mato (Inst. Inorg. Anal. and  
Phys. Chem., Zagreb Univ., Yugoslavia). *Bull. Sci.  
Fougat.*, 1956, 8 (1), 5 (in French).—The reagent  
is a saturated aq. soln. of nitrosobenzene kept at  
a pH of 4.1 by adding 0.1 vol. of 1 M acetate buffer.  
To a drop of this reagent are added 0.05 ml of the  
soln. containing  $Hg^{2+}$  and then 0.02 ml of aq.  
 $K_3Fe(CN)_6 \cdot 3H_2O$  (0.2%). The reactions are—  
 $Fe(CN)_6^{4-} + Hg^{2+} + H_2O \rightarrow$   
 $Fe(CN)_6H_2O^{2-} + HgCN^+$   
 $Fe(CN)_6H_2O^{2-} + C_6H_5NO \rightarrow$   
 $Fe(CN)_6NOC.H_5^{2-} + H_2O$   
(cf. *Brit. Abstr. A*, 1953, 493). The violet penta-  
cyanonitrosobenzene complex is determined spectro-  
photometrically. A blank test is carried out with  
water in place of the ferrocyanide solution. The limit  
of identification is 0.002  $\mu g$  of Hg, and the concn.  
limit 1 in  $25 \times 10^4$ . When present in concn.  
greater than that of  $Hg^{2+}$ , the ions  $Ag^+$ ,  $Au^{3+}$ ,  
 $Fe^{3+}$ ,  $Cu^{2+}$ ,  $UO_2^{2+}$  and  $I^-$  interfere.

A. R. PEARSON

25

Chem

MAT

✓ Photometric determination of microquantities of cyanides.  
 I. Kraljic and M. Mate (Univ. Zagreb, Yugoslavia). *Croat. Chem. Acta* 28:249-54 (1955) (in English).—A method based on the catalytic effect of  $Hg^{++}$  on the reaction of  $K_4[Fe(CN)_6]$  and  $PhNO$  (C.A. 49, 11376g) and on the measurement of the extinction of their violet reaction product  $[Fe(CN)_6NO]^{4-}$  was developed. The effects of pH, reaction time, concns. of  $Hg^{++}$ ,  $PhNO$  and  $K_4[Fe(CN)_6]$ , and temp. were investigated. For detg. the photometric calibration curve the following optimum concns. expressed as  $M/l$ .

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CIA-RDP86-00513R001032820006-9

*for  
any*

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CIA-RDP86-00513R001032820006-9"

MATE, 121

✓ 2524. A new sensitive and selective spot test for mercury.<sup>71</sup> Kraljic and M. Mate (Univ. Zagreb, Yugoslavia). Croat. Chem. Acta, 1959, 29 (4), 273-277 (in English).—The test is based on the catalytic effect of  $Hg^{2+}$  on the decomposition of  $Fe(CN)_6^{4-}$  in the presence of nitrosobenzene (cf. Anal. Abstr., 1957, 4, 2541) whereby the pink or violet water-sol.  $[Fe(CN)_5NO_2C_6H_5]^{3-}$  is formed. The sensitivity is 0.003  $\mu g$  of  $Hg$  (in 0.05 ml) or a limiting concn. of 1 in  $25 \times 10^4$ . Procedure—To one drop of sample soln. on a spot-plate, or in a test-tube, add one drop of a mixture (1 + 9) of acetate

buffer and saturated aq. nitrosobenzene, followed by one drop of a 0.5% soln. of  $K_3Fe(CN)_6 \cdot 3H_2O$ . Warm to 60°, adding another drop or two of nitrosobenzene if a spot-plate is used. Sufficient buffer should be present to maintain the pH at 4-5, and for concn. of  $Hg < 10^{-6} M$  a blank should be run simultaneously. Silver ( $> 2 \times 10^{-3} M$ ) and Au ( $> 10^{-3} M$ ) also give this reaction; other interfering cations ( $Fe^{3+}$ ,  $Cu^{2+}$ ,  $CO_3^{2-}$ ) can be suitably eliminated. Iodide in concn.  $> 10^{-3} M$  interferes seriously, but most other anions in concn. up to  $\approx 0.01 M$  can be tolerated. W. J. BAXTER

SM Jan 1960

YUGOSLAVIA/Analytical Chemistry - Analysis of Inorganic  
Substances.

E.

Abs Jour : Ref Zhur - Khimiya, No 9, 1958, 28490

Author : Kraljic, I. and Mate, M.

Inst : Yugoslav Academy of Sciences.

Title : A New Photometric Method for the Microdetermination of  
Cyanides.

Orig Pub : Bull scient Conseil acad RPFY, 3, No 3, 75 (1957) (in  
German)

Abstract : A new method is described for the determination of  $\text{CN}^-$ .  
The method is based on the inhibiting action of  $\text{CN}^-$  on  
the reaction between  $\text{Fe}(\text{CN})_6^{4-}$  and nitrobenzene, which  
is catalyzed by mercury. The concentration of the  
violet  $[\text{Fe}(\text{CN})_5\text{C}_6\text{H}_5\text{NO}]^{3-}$  complex formed in this reaction

Card 1/2

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MATE, Matyas, Dr.

On the training and refresher courses given to automobile traffic specialists. Auto motor 13 no.17:3 S '60.

1. A KPM Autoközlekedési Tanintézetnek igazgatója.

MATE, Matyas, dr.

What we have done and what we should do to reduce traffic  
accidents. Auto motor 14 no.4:3 F '61.

MATE, Matyas, dr.

Activity and tasks of the Automotive Transportation School,  
Ministry of Transportation and Posts. Autc motor 16 no.2:  
3-4 21 Ja '63.

1. Kozlekedes- es Postaugyi Miniszterium Autokozlekedesi Tanin-  
tezetenek igazgatoja.



MATE, Matyas, dr.

Activity and tasks of the School of Automotive Transportation of  
the Ministry of Transportation and Posts. Kozleked kozl 19  
no.4:54-56 27 Ja '63.

MATE, Sándor

Work competition in honor of the 8th Congress of the Hungarian  
Socialist Workers Party. Vasut 12 no.5:1 31 My '62.

MATE. Sender

Experiences of the international socialist work competition.  
Vasut 12 no.6:24 30 Je '62.

MATE, Sandor

Correlations between socialist competitions and objectives  
prescribed in the plan. Vasut 14 no. 4:4-7 Ap '64.

MATE, ~~Sandor~~ [Mata, Sandor] (Budapesht)

Professional training of railroad specialists in the Hungarian People's Republic. Zhel.dor.transp. 44 no.9:48-51 S '62.

1. Nachal'nik Upravleniya kadrov, truda i zarabotnoy platy zheleznikh dorog Vengerskoy Narodnoy Respubliki.

(Hungary--Railroads--Employees--Education and training)

MATE, Sandor; TESZERI, Gyorgy

Revision of wages for the workers of the Hungarian State  
Railways. Vasut 14 no. 1: 7-10 Ja '64.

MAE, Sander

Increasing labor productivity of the traveling personnel of traction  
and traction services. Vagut 14 no.9:8-9 5 '66.

MATE, Sh.

"The Effect of the Time of Plowing of Grass Layers on the Physicochemical Properties of Turf-Podzolic Soils and on the Yield of Later Crops." Cand Agr Sci, Leningrad Agricultural Inst, Min Higher Education USSR, Leningrad, 1955. (KL, No 14, Apr 55)

SO: Sum. No. 704, 2 Nov 55 - Survey of Scientific and Technical Dissertations Defended at USSR Higher Educational Institutions (160).



KASHSHAI, D' [Kassai, D.]; MATE, V.

Utilization of the vascular reaction to nicotinic acid for studying changes in the function of the nervous system in psychiatry. Zhur. nevr. i psikh 61 no.8:1232-1240 '61.

(MIRA 15:3)

1. Gosudarstvennyy neyro-psikhiatricheskiy institut (direktor i glavnyy vrach B. Mariya), Budapest.  
(BLOOD VESSELS) (NICOTINIC ACID) (NERVOUS SYSTEM)

KASHSHAI, D. [Kassai, D.]; MATE, V.

Effect of nicotinic acid on the skin temperature of patients with various states of schizophrenia. Zhur. nevr. i psikh. 61 no.11: 1688-1698 '61. (MIA 15:2)

1. Gosudarstvennyy neyropsikhiatricheskiy institut (direktor i glavnyy vrach B. Mariya), Budapesht.  
(NICOTINIC ACID--PHYSIOLOGICAL EFFECT)  
(SKIN) (SCHIZOPHRENIA) (BODY TEMPERATURE)

*Mate, Z.*  
HUNGARY / Chemical Technology, Cellulose and its  
Derivatives, Paper

H-33

Abs Jour: Ref Zhur-Khimiya, No 14, 1959, 51956.

Author : *Mate, Z.*

Inst : Not given.

Title : Utilization of New Raw Materials for Paper.

Orig Pub: Technika (Magyar), 1958, 2, No 12, 5.

Abstract: With the expansion of world production of paper, a respective expansion in the utilization of greater varieties of raw materials for its manufacture is also taking place. Deciduous varieties (particularly poplar), straw, etc., are now used. Presented are data pertaining to technological processes adapted to this type of raw material (particularly the monosulfite process); to the production of high yield pulp; to the developed continuous methods and

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MAGYAR, Imre.; VAGO, Erzsebet.; MATE, Zoltan.

Carbohydrate and kalium metabolism. 3. Effect of glycogen contents of the liver and the muscles on the kalium metabolism. Kiserletes orvostud. 7 no.1:66-72 Jan 55.

1. Budapesti Orvostudományi Egyetem I. sz. Belklinika.

(POTASSIUM, metabolism, eff. of glycogen contents in liver & musc.)

(GLYCOGEN

liver & musc., eff. on potassium metab.)

(LIVER, metabolism

potassium, eff. of glycogen contents)

(MUSCLES,

glycogen in, eff. on potassium metab.)

MAGYAR, Imre,; VAGO, Erzsébet,; MATE, Zoltan.

Carbohydrate and kalium metabolism. 4. Levulose and kalium.  
Kiserletes orvostud. 7 no.1:72-77 Jan 55.

1. Budapesti Orvostudományi Egyetem I. sz. Belklinika.  
    (FRUCTOSE, effects  
      on liver metab., relation to potassium)  
    (POTASSIUM, effects  
      on liver metab., relation to fructose)

MAGYAR, Imre, dr.; VAGO, Erzsébet, dr.; ~~MATE~~, Zoltan, dr.; GRASZ,  
Erzsébet.; SZUSZKAR, T. Judith, technikai segitsegevel.

Effect of euphyllin on hepatic circulation rate. Orv. hetil. 96  
no.11:287-290 13 Mar 55

1. A Budapesti Orvostudományi Egyetem I. sz. Belklinikájának  
igazgató: Rusznyak István dr. egyetemi tanár) közleménye.

(AMINOPHYLLINE, effects,  
on liver circ. rate)

(LIVER, blood supplh,  
eff. of aminophylline on circ. rate)

ZOMBORI, Janos, okleveles vegyeszmernok; MATE, Zoltan, okleveles  
vegyeszmernok

Complex utilization of wood. Technika 8 no. 6: 6-7 Je '64.

HUNGARY

ALDASY, Pal, Dr., Candidate of Veterinary Sciences, MATE, Zsuzsanna, Dr., and VANYI, Andras, Dr., of the Institute for Animal Hygiene (Allategeszsegugyi Intezet) in Miskolc (Director: ALDASY, Pal,)), and Directorate for the State Farms in Magye Borsod-Heves (Borsod-Heves Megyei Allami Gazdasagok Igazgatosaga)(Veterinarian-in-Chief: VANYI, Andras)[location not given].

"Investigations on the Viral Gastroenteritis in Pigs"

Budapest, Magyar Allatorvosok Lapja, Vol 21, No 6, Jun 1966, pp 247-251.

Abstract: A viral gastroenteritis epidemic occurred during the spring of 1965 in ten units of six State farms. This disease has not been previously observed in pigs in Northern Hungary. The findings were described and discussed with especial emphasis on epidemiological and diagnostic factors. After a period of about one month the epidemic subsided as fast as it broke out. It was not possible to trace the route of the infestation. Some histological data obtained in the investigations was presented. 14 references, including 1 German, 1 Japanese, 3 Hungarian, and 9 Western.

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KOROS, Zoltan, dr.; HARTAI, Ferenc, dr.; MATE-WOJCINSKA, Urszula; SELLEI, Camillo, dr.

Data on the mechanism of action of Degranol. Magy 6nk. 8 no.1: 18-23 Mr'64.

1. Az Orszagos Onkologiai Intezet Belosztalya laboratoriumna es a Chinoin Gyogyszer es Vegyeszeti Termekek Gyara Technologiai laboratoriuma.

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MATECKI, J.

The organization of active rest for flying personnel on flight days. P. 11.

WOJSKOWY PRZEGLĄD LOTNICZY. (Dowództwo Wojsk Lotniczych) Warszawa, Poland.  
Vol. 12, no. 3, Mar. 1959.

Monthly list of East European Accessions (EEAI) IC, Vol. 1, no. 7, July 1959.

Uncl.

KLIMEK, Rudolf; MATECKI, Tadeusz

Primary ovarian pregnancy. Gin. polska 32 no.4:449-453 '61.

1. Z I Kliniki Położnictwa i Chorob Kobietych AM w Krakowie Kierownik:  
prof. dr S. Szwarc Z Zakładu Anatomii Patologicznej AM w Krakowie  
Kierownik: prof. dr J. Kowalczykowa  
(PREGNANCY ECTOPIC case reports)

SCHWARZ, Stefan. ZAMELLO, Henryk. KLIMEK, Roman. MARCZYNSKI, Kazimierz.  
MATECKI, Jacek. MILEWICZ, Stanislaw. SOLARZ, Edward

Statystyka w chorobach zakaźnych i pasożytach. Podręcznik dla lekarzy. Ośrodek  
Badań i Dosлідzeń w dziedzinie Chorób zakaźnych i Medycyny  
Kraków. Instytut Medycyny. 1978. 112 s. 11 cm. 11 cm. 11 cm. 11 cm.  
Ja-F'04

1. Z I Kliniki Polon. w Krakowie. AM - Kraków.  
kierownik: prof. dr. med. S. S. 1978.

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6.3230/1040, 1139, 1147)

R/005/62/000/001/002/003  
D014/D105

AUTHOR: Mateescu, Adelaida, Engineer

TITLE: Considerations on modern designing methods of electric filters

PERIODICAL: Telecomunicatii, no. 1, 1962, 25 - 30

TEXT: The article briefly presents the principles of modern electric filter theories without taking into consideration the problems of transition conditions, the approximation of the phase characteristics, the time synthesis, the influence of losses and the case of some special filters. To design a filter with a given behavior, the following technical requirements have to be fulfilled: (1) optimum approximation of the attenuation or transfer characteristics given with a frequency function, to which a real electric circuit should correspond; (2) synthesis of the function which approximates the characteristic given under the shape of a physically realizable electric circuit; and (3) selection of the most adequate circuit. The method of frequency transformation is often used in the synthesis of electric filters. When the synthesis of low-pass filters has been worked out, the solution obtained can also be

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Considerations on modern designing methods ...

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applied for other types of filters. The first step in designing a filter is the approximation of the filter characteristics. The problem may be solved by using the Chebyshev criterion. The position of the poles established by a supplementary condition, i.e. the absolute value of the fractions standardized by Chebyshev

$$\hat{F}(x) = \cos \left[ (l+1) \arccos x + \sum l_k \arccos \frac{\alpha_k x - 1}{\alpha_k - x} \right], \quad (6)$$

valid within the approximation field, or

$$\hat{F}(x) = \cos \left[ (l+1) \operatorname{Ar} \operatorname{ch} x + \sum l_k \operatorname{Ar} \operatorname{ch} \frac{\alpha_k x - 1}{\alpha_k - x} \right], \quad (7)$$

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Considerations on modern designing methods ...

valid for values beyond the approximation field, should not drop beyond the approximation field below the given limit  $\lambda$ . This problem may be solved by the so-called "third problem of Zolotarev". The most frequently used parameters for the determination of the filters are (a) working parameters, and (b) image parameters. The article deals only with symmetric and antisymmetric filters. The author briefly describes the calculation of electric filters by these two methods and refers to S. Cogan who recently established some formulas for the technical calculations of the image parameters. Comparing the two methods, the author came to the conclusion that the optimum variation of the echo attenuation in the pass-band may be selected by the working attenuation method. By the image-parameter method, the optimum variation of the echo attenuation in the pass-band is obtained by selecting the cell with the optimum image impedance, without obtaining a Chebyshev-type behavior for the composed attenuation  $a_c$  in the pass-band. In the stop-band, both methods lead to optimum characteristics. Although from the performance point of view the designing of filters by the composed attenuation is more advantageous, the great number of complicated calculations represents a draw-back. The image-

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Considerations on modern designing methods ... R/005/62/000/001/002/003  
DQ14/D105

parameter method is simpler and faster, and may be used where no exceptional performances are required. There are 7 figures and 4 references: 2 Soviet-bloc, 1 non-Soviet-bloc and 1 unidentified. The reference to the English-language publication reads as follows: W. Cauer, "Synthesis of Linear Communication Networks", Mc Graw-Hill, Book Comp. Inc., London, 1958.

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Card 4/4



MATEESCU, Adelaida, ing.

Influence of the variation of elements on the parameters of the picture,  
in dephasing X circuits. Telecomunicatii 7 no.1:18-25 Ja-F '63.

I 1220-66

ACCESSION NR: AP5025823

RU/0005/65/000/004/0106/0113  
16

AUTHOR: Mateescu, Adelaida (Engineer)

TITLE: Susceptibility of the all-pass circuit operating parameters to the variation of circuit elements

SOURCE: Telecommunicatii, no. 4, 1965, 106-113

TOPIC TAGS: circuit theory, circuit design

ABSTRACT: The effect of small variations in circuit elements on the operating parameters of all-pass circuits. The author shows how to calculate the degradation of the circuit parameters with time if the variation with time of the components (e.g., wearing out) is known, as well as how to calculate allowable tolerances for the components in terms of the desired circuit parameters. Orig. art. has: 5 figures, 69 formulas and 4 graphs.

ASSOCIATION: none

SUBMITTED: 00

ENCL: 00

SUB CODE: EC

NR REF SOV: 002

OTHER: 011

JPRS

Card 1/1 *mcb*

MATEESCU, C.

TECHNOLOGY

PERIODICAL: REVISTA INDUSTRIEL ALIMENTARE. PRODUSE VEGETALE No. 7<sup>9</sup> 1958

MATEESCU, C. How preparations developed in the Chitila Sugar Plant in view of the new production drive. p. 26

Monthly List of East European Accessions (EEAI) LC Vol. 8, No. 1  
April 1959, Unclass

MATEESCU, C.

To what extent the Cicoarea Plants are prepared for the winter season. P 26

REVISTA INDUSTRIEI ALIMENTARE. PRODUSE VEGETALE. (Ministerul Industriei  
Bunurilor de Consum si Sindicatul Muncitorilor din Industria Bunurilor de  
Consum) Bucuresti, Rumania. No. 12, 1958

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Uncl.



MATELSCU, C.

Functional indices for economic computation of dams. p. 49

Vol. 2, no. 2, Feb. 1954

ENERGETICA

Bucuresti

Source: East European Accessions List (EAL), LC, Vol, 5, No. 2  
Feb. 1956

MATEESCU, C.; VLADIMIRESCU, I. ; BOISNARD, J.

General considerations on the economy of Rumanian waters. p. 152.  
(HIDROTECHNICA, Vol. 2, no. 4, July/Aug. 1957, Rumanian)

SO: Monthly List of East European Accessions (EEAL) LC. Vol. 2, No. 12, Dec. 1957  
Uncl.

MATEESCU, C.

TECHNOLOGY

Periodicals: HIDROTEHNICA. Vol. 3, no. 2, Sept. 1958

MATEESCU, C. Critical considerations concerning the calculation of concrete dams. p. 325

Monthly List of East European Accessions (EEA) LC, Vol. 8, No. 2,  
February 1959, Unclass.



MATEESCU, C..

Synoptic study of superrelaxation methods for concrete barrages. p. 1

HIDROTEHNICA. (Asociatia Stiintifica a Inginerilor si Tehnicienilor din Romania) Bucuresti, Rumania Vol. 4, no. 1, Jan. 1959

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Uncl.

MATEESCU, Ch

MATEESCU, Kriatya [Mateescu, Ch.]

Lights on the Byetritsa. Hauka i zhyttia 10 no.5:49-52 My '60.  
(MIRA 13:7)

1. Chlen-korrespondent AN Rumynskoy Narodnoy Respubliki.  
(Rumania--Hydroelectric power stations)

MATERESCU, Cristea, prof. dr. ing.; VLADIMIRESCU, Ion, conf. ing.;  
TROFIN, Elena, sef lucrari ing.; BRATU, Cristian, asist. ing.

Contributions to the study of drainage of the water infiltration  
in the Danube flood plain in a dam-controlled regime of the river.  
Hidrotehnica 7 no. 12:409-417 D '62.

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Problems of the economical design of hydraulic structures. Studii  
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1. Membru corespondent al Academiei R.P.R.

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MATEESCU, C.

A study of the distribution of speeds in the uniform flow of viscous fluids by the method of flow tubes and the curvilinear networks. p. 863.

COMUNICARILE. Bucuresti, Rumania, Vol. 7, no. 10, October 1957

Monthly List of East European Accessions (EEAI) LC Vol. 8, no. 8, August, 1959

Uncl.

MATEESCU, C.

New methods for determining the distribution of speeds in the uniform flow of viscous fluids. p. 991.

Academia Republicii Populare Romine. Institutul de Mecanica Aplicata.  
STUDII SI CERCETARI DE MECANICA APLICATA. Bucuresti, Rumania. Vol. 8, no. 4,  
1957.

Monthly list of East European Accessions (EEAI) LC, Vol. 8, no. 8, Aug. 1959

Uncl.



Distr: 4E4

✓ 2990. Mutseanu, Ct., New methods for the determination of velocity distribution in steady laminar flow of viscous fluids (in English), *Acad. Repub. Pop. Romina, Rev. Mecan. Appl.* 3, 2, 41-60, 1958.

Paper concerns the determination of velocity distribution in the laminar flow of a viscous fluid, through approximate methods applicable to steady motions. A first procedure proposed belongs to the general class known as relaxation methods and uses a curvilinear network. Each mesh of this network is considered to be the cross section of a stream tube. The finite difference equations are obtained directly from the motion equations written for each of these tubes. The approximations introduced are then discussed and a few examples are given.

The second procedure consists in superimposing two steady uniform motions in rectilinear tubes, having the same piezometric line and the same viscosity. The velocity distribution for motions whose boundaries differ from those of the initial motions is thereby obtained. Considerations on the equal velocity curves are finally presented.

T. Oroveanu, Roumania

RUMANIA / Chemical Technology. Chemical Products and      H  
Their Application, Chemical Engineering.

Abs Jour: Ref Zhur-Khimiya, No 12, 1959, 42588.

Author : Mateescu C.

Inst : Not given.

Title : Certain Properties of Constant Velocity Flow Pat-  
terns in the Movement of Liquids Through Pipes and  
Channels.

Orig Pub: Comun. Acad. RPR, 1958, 8, No 5, 479-485.

Abstract: Characteristics of constant velocity flow patterns  
are reviewed for cross sectional areas involved in  
viscous and turbulent flow of liquids. A method  
of plotting such characteristics based on the flow  
rate results is presented. -- Z. Khaimskiy.

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MATEESCU, D.; BOTA, V.; ROSU, D.

Suspended system for passing the gas conduct over the  
Mures River. Bul St si Teha Tim 7:265-276 '62.

Reconstruction of a forge hall, a construction with metallic  
framework. Ibid.:277-286

MATEESCU, Dan, prof. ing.; FLESERIU, I.; FLESERIU, E.; GADEANU, L.;  
BOTA, V.; ROSU, D.; FILIMON, I.; MAIOR, N.; IZDRAILA, V.;  
PAUNESCU, M.; ROSA, Sidonia

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of some apartment houses with metallic framework of light elements.  
Pt. 1-3. Bul St si Tehn Tim 7:287-321 '62.

MATEESCU, D.

Scheme for rationalization of the assortment of laminated products. p. 162.

Vol. 7, no. 234, June 1955  
CONSTRUCȚIIL  
Bucuresti, Rumania

Source: East European Accession List. Library of Congress  
Vol. 5, No. 3, August 1956

MATEESCU, D.

TECHNOLOGY

REVISTA CONSTRUCTILOR SI A MATERIALELOR DE CONSTRUCTII. Vol. 10, no. 9,  
Sept. 1958.

The optimum height for truss girders. p.588.

Monthly List of East European Accessions (EEAI), LC, Vol. 8, No. 1, 2  
~~May~~ 1959, Unclass.  
Hansen

MATINESCU, D.; CARAFOLI, E.

Supersonic flow around the system carrying a conic wing fuselage. In French. p.377.

REVUE DE MECANIQUE APPLIQUEE. (Academia Republicii Populare Romane.  
Institutul de Mecanica Aplicata)  
Bucuresti, Rumania  
Vol. 4, no. 3, 1954.

Monthly list of Eastern European Accession Index (MEAI) LC vol. 1, no. 11  
November 1959  
Uncl.

106120

R/008/60/000/001/001/009  
A125/A026AUTHORS: Carafoli, Elie and Mateescu, DanTITLE: General Method of Determining the Interference of Wing and Conical Fuselage in Supersonic Regime

PERIODICAL: Studii și Cercetări de Mecanică Aplicată, 1960, No. 1, pp. 11-47

TEXT: In a previous work (Ref. 1), the authors presented a method of solving the problem of supersonic flow around a wing/conical fuselage system. In subject article, this method is extended to the case of a wing with edges on which there are incidence and inclination leaps, thus establishing a general method of solution of the supersonic flow around the wing/conical fuselage system. Considered is a wing/fuselage system (Fig. 1), where the fuselage axis has the incidence  $\alpha_0$  against the undisturbed flow  $U_\infty$ , and the wing has a constant incidence and inclination. The authors assume that the fuselage has reduced dimensions against the Mach cone ( $B^2 c^2 \ll 1$ ), that the incidence and the inclination, as well as the  $\alpha_0$  incidence of the fuselage are small enough for the application of the theory of small disturbances. The stream around this system can be decomposed into: 1) symmetric axial stream around the isolated

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A125/A026

General Method of Determining the Interference of Wing and Conical Fuselage in Supersonic Regime

conical fuselage without incidence; II) motion around the conical fuselage/thin wing system; and III) motion around the conical fuselage/symmetric thick wing system. The authors treat the last two motions and first present the usual notations and formulae. For the solution of the problem they deduce the boundary conditions of the function  $\psi$ . Based on the function (13) and the compatibility relation, the solution of the motion is expressed by (14). The boundary conditions are now more simple and can be expressed by (15), (16), (17) and (18). Based on the conform transformation (3), the relation (19) is obtained for the X plane, from which result the boundary conditions (20), (21), (22) and (23) in the X-plane (Figs. 3a, b, c). The function  $\psi_a$  presents the same singularities (24), (25) and (26), and satisfies the boundary condition (23) as the function  $\frac{d\psi}{dx}$ , thus:  $\frac{d\psi}{dx} = \psi_a$ , (29). Replacing  $\frac{d\psi}{dx}$  by its value from (19) in the relation (14), the axial disturbance speed  $u$ , which is a real part of the expression (30) is obtained.  $\psi_a$  and  $\psi_a$  of this expression represent the solution of the conical stream around the fictive wing. Thus, the problem of the supersonic stream around the wing/conical fuselage system has been re

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General Method of Determining the Interference of Wing and Conical Fuselage in Supersonic Regime

duced to a conical stream around a fictive, isolated wing with variable incidence. In paragraph 3, the authors determine the solution of the problem for different particular cases selected in such a way that, adding the effects, the solution of the general case of the wing/conical fuselage system could easily be determined if the wing incidence is constant on the sections. They first treat the case, where the whole system has the same incidence and then some cases where the wing has incidences on the sections which are different from that of the wing. The following particular cases are examined: 1) The wing and the fuselage have the same  $\alpha_0$  incidence; 2) The wing has an  $\alpha_0$  incidence on the  $M_1A_1$  section, the rest of the wing and the fuselage axis having no incidence; 3) The wing has an incidence  $\alpha_2$  on the  $A_2M_2$  section, the rest of the wing and the fuselage axis having no incidences; 4) The wing has an  $\alpha$  incidence on the  $A_2M_2$  and  $A_1M_1$  sections, the rest of the wing and the fuselage axis having no incidence; 5) The whole wing has an  $\alpha$  incidence, the fuselage axis having no incidence; and 6) Application examples, where the authors present the expressions of the axial-disturbance speeds for the most interesting cases. Finally

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General Method of Determining the Interference of Wing and Conical Fuselage in  
Supersonic Regime

they treat the motion around a conical fuselage/symmetric thick wing system  
(Fig. 4). There are 3 figures and 3 references: 1 Rumanian, 1 English and  
1 Austrian (German). ✓c

SUBMITTED: October 29, 1959

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10 6120 3515, 2310, 2207

R/008/60/000/002/001/007  
A125/A026

AUTHORS: Carafoli, Elie, and Mateescu, Dan  
TITLE: Supersonic Flow Around a Conical Cross-Wing/Fuselage System  
PERIODICAL: Studii și Cercetări de Mecanică Aplicată, 1960, No. 2, pp. 325-337

TEXT: The authors treat the problem of flow around a conical cross-wing - fuselage system provided with a normal plate (Fig. 1), for the case where the leading edges of the wing and of the plate are subsonic and the angle of incidence of the fuselage differs from those of wing and normal plate. The study starts from the hypothesis of minor disturbances, taking into account that the dimensions of the fuselage are small enough in relation to the Mach cone, and that the angles of incidence of wing, normal plate and fuselage are also sufficiently small. The general flow around the system investigated is decomposed into three movements: the 1st is the axial-symmetric flow around the bare conical fuselage - which is known -, the 2nd is the flow around the system symmetric plate/fuselage - which was the object of another paper by the same authors (Ref. 1), and the last one is the flow around the system cross-wings/fuselage, with the plate and the fuselage being without lateral angles of incidence; this latter movement is the sub-

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R/008/60/000/002/001/007  
A125/A026

Supersonic Flow Around a Conical Cross-Wing/Fuselage System

ject of this paper. The problem is referred to a conveniently chosen plane where it is reduced to the problem of determining two simple movements: a conical one around a very thin cross-wing, and a plane one around a circle. The authors give the general expression for the axial speed of disturbance  $u$ , indicating the method of determining the constants. There are 3 figures and 4 Rumanian references; 2 of these were published in English and 2 in French.

SUBMITTED: February 12, 1960

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R/008/60/000/001/001/009  
D256/D301

AUTHORS: Carafoli, Elie, and Mateescu, Dan

TITLE: A general method for determining the interference between the wing and conical fuselage in a supersonic state

PERIODICAL: Studii și cercetări de mecanică aplicată, no. 1, 1960, 11-47

TEXT: In a previous work, the authors (Ref. 1: Scurgerea supersonică în jurul sistemului portant aripă-fuzelaj conic (Supersonic Flow around a Wing-Conical Fuselage Lifting System), Studii și cercetări de mecanică aplicată, X, 2, 1959) presented a method of solving the problem of supersonic flow around a wing-conical fuselage lifting system. In the present article this method is extended to the case of a wing with edges, on which there are incidence and inclination leaps, thus establishing a general method of solv-

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ing the wing-conical fuselage system. Considered is a wing-fuselage system as shown in Fig. 1, the fuselage axis having an angle of attack  $\alpha_0$  against the non-disturbed flow  $U_\infty$ , and the wing having a constant angle of attack and inclination. The authors assume that the fuselage has low dimensions against the Mach cone, i.e.  $B^2 c^2 \ll 1$ , that the angle of attack and the inclination, as well as the  $\alpha_0$  angle of attack of the fuselage are small enough to apply the theory of small disturbances. In this case, the stream around this system can be broken down into: I) symmetric axial stream around the isolated conical fuselage without angle of attack; II) motion around the conical fuselage - thin wing system; and III) motion around the conical fuselage - symmetric thick wing system. The authors treat the last two motions:  $U_\infty$  = velocity of the undisturbed flow;  $a_\infty$  = speed of sound in infinite conditions;  $M_\infty = \frac{U_\infty}{a_\infty}$  : Mach number;  $B = \sqrt{M_\infty^2 - 1}$ ;  $Ox_1x_2x_3$  = system of orthogonal

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coordinates, the  $Ox_1$  axis being directed according to the fuselage axis (Fig. 1);  $y = \frac{x_2}{x_1}$ ,  $z = \frac{x_3}{x_1}$  : coordinates of the  $oyz$  physical plane ( $x_1 = 1$ , Fig. 1);  $\omega\eta\xi$  = Busemann's plane, obtained by transformation

$$Br = \frac{2\rho}{1+\rho^2}, \theta = 0, (r^2 = y^2 + z^2, \rho^2 = \eta^2 + \zeta^2); \quad (1) \quad (1)$$

$oyz$  = auxiliary plane obtained by the conform transformation:

$$Bx = \frac{2\xi}{1+\xi^2}, (x = y + iz, \xi = \eta + i\zeta); \quad (2) \quad (2)$$

OYZ = auxiliary plane obtained by the conform transformation:

$$X = \omega + \frac{c^2}{z}, \omega = \frac{x + \sqrt{x^2 - 4c^2}}{2}, X = Y + iZ, \quad (3) \quad (3)$$

in which  $c$  is the radius of the circular section of the fuselage

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in the  $x_1 = 1$  plane;  $u, v, w$  = components of disturbance speed according to the  $Ox_1, Ox_2, Ox_3$  axes which are harmonic functions in the  $\xi, x, X$  planes; and  $U = u + iu', V = v + iv', W = w + iw'$  : analytic functions, between which the compatibility relations

$$dU = -x dV = \frac{ix dW}{\sqrt{1 - B^2 x^2}} \quad (4)$$

can be written. The authors then present the calculation method, considering the conical fuselage - thin wing system, the fuselage axis having an  $\alpha_0$  angle of attack, and the wing an  $\alpha_i$  angle of attack constant on the portions ( $i = 1, 2, 3, \dots$ ). The wing has the leading edge in  $A_1$  ( $y = l_1, z = 0$ ), and  $A_2$  ( $y = -l_2, z = 0$ ) and has incidence leaps on the edges from the points  $M_i$  ( $y = s_i, z = 0$ ), in which  $i = 1, 2, 3, \dots$ . The boundary conditions in this case are:

$$\cos \theta + (w - \alpha_0 U_\infty) \sin \theta \approx 0, \quad (5)$$

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on the circle of a  $c$  radius which represents the trace of the fuselage in the  $oxy$  physical plane, and

$$w = \alpha_i U_\infty = \text{const.}, \quad (i = 1, 2, 3, \dots), \quad (6)$$

on different portions of the wing's trace. The boundary conditions on the rest of the  $oxy$  axis and on the Mach circle are the same as in the case of an isolated thin wing. The disturbance speeds  $u$  and  $v$  have the same peculiarities on the leading edges of the wing which represent incidence leaps, as in case of the isolated thin wing. Thus, the functions  $U = u + iu'$  and  $V = v + iv'$  tend towards infinite in these points as expressions:

$$\frac{1}{\sqrt{l_1 - x}}, \quad \frac{1}{\sqrt{l_2 + x}}, \quad (7)$$

if the leading edges are subsonic; or as expressions:

$$\ln(l_1 - x), \quad \ln(l_2 + x) \quad (8)$$

if the leading edges are supersonic; and finally as expressions:

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$$\ln (s_1 - x) \quad (9)$$

if there is an edge located in the  $x = s_1$  point. To solve the problem, the authors deduce the boundary conditions of the function  $\mathcal{U}$ . Based on the compatibility relations (4) and still considering the fuselage section's radius in the  $oyz$  physical plane being very small against the Mach circle, they deduce

$$-dv' \approx dw, \quad v' + w = k_0 = \text{const.} \quad (10)$$

on the circle with a radius  $c$ , in the  $x$  plane, as shown in Fig. 2 a, b, c. Taking, on the other hand, relation (6) into consideration, they deduce

$$-dv' = \frac{dw}{\sqrt{1 - B^2 v^2}} = 0, \quad v' = k_i = \text{const.}, \quad (i = 1, 2, 3, \dots, n) \quad (11)$$

on different subsonic portions of the wing, and

$$dv = \frac{dw}{\sqrt{B^2 v^2 - 1}} = 0, \quad v = K_j = \text{const.}, \quad (j = n+1, n+2, \dots), \quad (12)$$

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on different supersonic portions of the wing. Considering as in  
(Ref. 1:Op.cit.) function

$$\frac{dF}{dz} = 0 - i(k_0 - \alpha_0 U_\infty), \quad (13) \quad (13)$$

and relation (4), the solution of the motion will be expressed by

$$u = -x \frac{dF}{dz} + F. \quad (14) \quad (14)$$

The boundary conditions are now simpler and can be expressed by

$$\operatorname{Re} x \frac{dF}{dz} = 0 \quad (15) \quad (15)$$

on the circle of a radius c, or by

$$\operatorname{Im} \frac{dF}{dz} = K_i = \text{const.}, \quad (i = 1, 2, 3, \dots, n), \quad (16) \quad (16)$$

on different portions of the segment  $(\max \left[ -\frac{1}{B}, -1_2 \right] < y < -c,$

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$z = 0$ ), or of the segment ( $c < y < \min \left[ -\frac{1}{B}, l_1 \right]$ ,  $z = 0$ ); or by:

$$\operatorname{Re} \frac{dF}{dz} = K_j = \text{const.}, \quad (j = n+1, n+2, \dots), \quad (17)$$

on different portions of the segment ( $-l_2 < y < -\frac{1}{B}$ ,  $z = 0$ ), if  $l_2 > \frac{1}{B}$ , or on the segment ( $\frac{1}{B} < y < l_1$ ,  $z = 0$ ), if  $l_1 > \frac{1}{B}$ ; and finally by

$$\operatorname{Re} \frac{dF}{dz} = 0 \quad (18)$$

on the semi-straight-lines ( $y < -l_2$  and  $y > l_1$ ,  $z = 0$ ). Based on transformation (3), relation

$$\frac{dF}{dX} = \alpha \frac{dF}{dz} \frac{1}{x - \frac{c^2}{x}} = \frac{1}{2} \left( 1 + \frac{X}{\sqrt{X^2 - 4c^2}} \right) \frac{dF}{dz}, \quad (19)$$

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is obtained for the X plane, whence result the boundary conditions:

$$\operatorname{Im} \frac{dF}{dX} = 0 \quad (20)$$

on the  $(-2c < y < 2c, Z = 0)$  segment;

$$\operatorname{Im} \frac{dF}{dX} = \frac{K_1}{2} \left( 1 + \frac{Y}{\sqrt{Y^2 - 4c^2}} \right), \quad (i = 1, 2, \dots, n), \quad (21)$$

on the different portions of the segments  $(\max \left[ -\frac{1}{B}, -L_2 \right] < Y < -2c, Z = 0)$  and  $(2c < Y < \min \left[ L_1, \frac{1}{B} \right], Z = 0)$ ;

$$\operatorname{Re} \frac{dF}{dX} = \frac{K_1}{2} \left( 1 + \frac{Y}{\sqrt{Y^2 - 4c^2}} \right), \quad (j = n + 1, n + 2, \dots) \quad (22)$$

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on the different portions of the segments  $(-L_2 < Y < -\frac{1}{B}, Z = 0)$ ,  
if  $L_2 > \frac{1}{B}$ , and  $(\frac{1}{B} < Y < L_1, Z = 0)$ , if  $L_1 > \frac{1}{B}$ ; and finally

$$\operatorname{Re} \frac{dF}{dX} = 0 \quad (23)$$

on the semi-straight-lines  $(Y < -L_2 \text{ and } Y > L_1, Z = 0)$ . For the  
function  $\frac{dF}{dX}$ , there result in the corresponding points of the lea-  
ding edges the peculiarities

$$\frac{1}{\sqrt{L_1 - X}}, \quad \frac{1}{\sqrt{L_2 + X}} \quad (24)$$

if the leading edges are subsonic, and respectively  
 $\ln (L_1 - X), \ln (L_2 + X),$  (25)

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if the leading edges are supersonic, as well as  
 $\ln (S_1 - X)$  (26)

in the leap points  $X = S_1$ . The magnitudes  $L_1$ ,  $L_2$  and  $S_1$  are given

by  
 $L_1 = l_1 + \frac{c^2}{l_1}$ ,  $L_2 = l_2 + \frac{c^2}{l_2}$ ,  $S_1 = s_1 + \frac{c^2}{s_1}$ . (27)

Considering now in the  $X$  plane a fictive conical motion with the disturbance speeds  $u_a = Re U_a$ ,  $v_a = Re V_a$  and  $w_a = Re W_a$ , which satisfy the relations

$$dU_a = -X dV_a = \frac{(X dW_a)}{\sqrt{1-B^2 X^2}}, \left( \frac{1}{B} = \frac{1+B^2 X^2}{B} \right). \quad (28)$$

also considering that the leading edges of the fictive wing are located in the same points  $X = L_1$  and  $X = -L_2$  and that the fictive

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wing has the same edges in the points  $X = S_1$  ( $i = 1, 2, 3, \dots, n$ ), the  $U_\alpha$  function presents the same peculiarities (24), (25) and (26) and satisfies the same boundary conditions (23) as the functions  $\frac{dF}{dX}$ , thus:

$$\frac{dF}{dX} = U_\alpha, \quad (29)$$

Replacing in the relation (14)  $\frac{dF}{dX}$  by its value from (19), one obtains the axial disturbance speed  $u$ , which is a real part of

$$u = U_\alpha + \frac{2c^2}{X} U_\alpha, \quad (30)$$

in which  $U_\alpha$  and  $V_\alpha$  represent the solution of the conical flow around the fictive wing. Thus, the problem of the supersonic flow around the wing - conical fuselage system is reduced to a conical flow around a fictive, isolated wing with variable angle of attack.

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The authors then determine the solution of the problem for different particular cases selected in such a way that, by adding the effects, the solution of the general case of the wing-conical fuselage system could easily be determined if the wing's angle of attack is constant on the sections. The following cases are treated: 1) The wind and the fuselage have the same angle of attack  $\alpha_0$ ; 2) The wing has on the  $M_1A_1$  section an angle of attack  $\alpha_1$ , the rest of the wing and the fuselage's axis having no angle of attack; 3) The wing has on the  $A_2M_2$  section an  $\alpha_2$  angle of attack, the rest of the wing and the axis of the fuselage having no angle of attack; 4) The wing has the same angle of attack  $\alpha$  on the  $A_2M_2$  and  $M_1A_1$  sections, the rest of the wing and the fuselage's axis having no angle of attack; 5) The whole wing has an angle of attack of  $\alpha$  and the fuselage's axis having no angle of attack. By using the principle of adding the effects, one may easily determine the solution in the general case when the wing's angle of attack is con-

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stant on the sections: a) If the whole wing has the same angle of attack  $\alpha$ , and the fuselage has an angle of attack  $\alpha_0$ , the axial disturbance speed is given by

$$u = \frac{c_0 l_1 l_2 \left(1 + \frac{c^2}{l_1^2}\right) \left(1 + \frac{c^2}{l_2^2}\right) - 2c^2 \left(1 + \frac{c^2}{x^2}\right) + \frac{l_1 - l_2}{2} \left[ \left(1 - \frac{c^2}{l_1 l_2}\right) \left(x + \frac{3c^2}{x}\right) + \frac{2c}{\pi} \frac{x}{c_0} \sqrt{l_1 l_2} \left(x - \frac{c^2}{x}\right) \right]}{\sqrt{(l_1 - x)(l_2 + x)} \sqrt{\left(1 - \frac{c^2}{l_1 x}\right) \left(1 + \frac{c^2}{l_2 x}\right)}} \quad (91)$$

$$- \frac{2xc}{\pi} \left(1 - \frac{c}{x}\right) \arg \operatorname{ch} \sqrt{\frac{(L_1 - X)(L_2 + 2c)}{(L_1 + L_2)(2c - X)}} -$$

$$- \frac{2xc}{\pi} \left(1 + \frac{c}{x}\right) \arg \operatorname{ch} \sqrt{\frac{(L_2 + X)(L_1 + 2c)}{(L_1 + L_2)(2c + X)}} - \frac{ixc^2}{x}, \quad (91)$$

in which  $x$ , however, has the value of

$$x = \frac{(\alpha_0 - \alpha) U_\infty}{\sqrt{1 - B^2 c^2}} \quad (94)$$

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b) If the wing has an angle of attack  $\alpha_1$  on the  $A_2M_2$  and  $M_1A_1$  sections and an angle of attack  $\alpha_2$  on the  $M_2N_2$  and  $N_1M_1$  sections, and the fuselage has an angle of attack  $\alpha_0$ , as well as the wing having a geometrical symmetry against the fuselage axis, i.e.  $l_1 = l_2 = l$ , and  $s_1 = s_2 = s$ , the solution where the leading edges are subsonic is given by

$$u = \frac{C + 2c^2D' + C'x + (C' + 2D) \frac{c^2}{x} + 2D' \frac{c^4}{x^2}}{\sqrt{1^2 - x^2} \sqrt{1 - \frac{c^4}{l^2 x^2}}} - \frac{2\pi c}{\pi} \left(1 - \frac{c}{x}\right) \arg \operatorname{ch} \sqrt{\frac{(L - X)(L + 2c)}{2L(2c - X)}} - \frac{2\pi c}{\pi} \left(1 + \frac{c}{x}\right) \arg \operatorname{sh} \sqrt{\frac{(L + X)(L + 2c)}{2L(2c + X)}} - \frac{ixc^2}{x} -$$

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